# HBM2 - Reference Manual





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# Preface

Motek provides innovative products for rehabilitation, orthopedics, neurology, performance enhancements and research. Motion platforms, instrumented treadmills, motion-capture systems and surround sound are combined with integrated Virtual Reality (VR) environments to train movement functions and improve (dynamic) stability.

We hope you will enjoy using the HBM and that it helps you to improve clinical care.

Regards, Motek

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# **1.Introduction**

This document describes the Human Body Model (HBM) software by Motek, which was originally described by van den Bogert et al. (2013). The model is designed for real-time biomechanical analysis of joint kinematics and kinetics, as well as estimation and visualization of muscle function. HBM was updated in 2017 to meet the current state of the art in the field of gait analysis and biomechanical research.

Marker movement and (ground) reaction forces are measured and provided as input in a biomechanical model to calculate the joint torques produced by the skeletal muscles. The HBM model takes it one step further by using an optimized muscle model to calculate muscle forces. These real-time calculated muscle parameters and motion variables can be used to provide immediate feedback to both operator and subject.

Kinematic analysis is done using a global optimization method. This makes the model less sensitive to marker drop-outs and skin artifacts, which are inevitable in motion capture.

The muscle model used in HBM contains information on muscle locations and parameters which is not subject specific, but based on data of healthy adults. This needs to be taken into consideration when using the muscle outputs of the model in subjects in which the control of muscles or the parameters of the muscle have changed.

#### Changes in the 2017 update

Originally, HBM was initialized by recording an initialization pose in which subjects had to stand straight and symmetrically, with feet pointing forward. However, not all subjects are able to assume this pose due to for example spasms or bone deformities. This might lead to incorrect locations of the knee and ankle joint axis and therefore incorrect data. The updated HBM uses medial markers on the knee and ankle to make the model initialization less pose dependent. Furthermore, joint centers of the knees and hips can now also be estimated using functional calibration methods. All changes incorporated in the updated model are listed below:

- The predictive method used in hip joint estimation is changed from the method proposed by Bell et al. (1989) to linear regression equations proposed by Harrington et al. (2007).
- The proximal trunk joint has been relocated to the T10/T11 joint based on data from Bruno et al. (2015).
- Medial epicondyle and medial malleolus markers (LMEK, RMEK, LMM and RMM) are added. These markers are only used during calibration and can be removed during the walking trial.
- Segment definitions have been changed to match ISB recommendations (Wu et al. 2005) and clinical gait analysis practice more closely (see Section 4).
- Functional hip and knee calibration procedures, using separate range of motion trials, to determine hip and knee joint center and knee joint axis are available.
- Muscle volume weighting is now applied in muscle solver.
- Internal muscle model updated to gait2392 model (Delp et al. 2007).

Changes in marker set

- The BBAC marker is removed from the markerset
- LGTRO and RGTRO (greater trochanter) markers are removed to avoid soft tissue artifacts associated with this marker.
- SACR (sacrum) and NAVE (navel) markers are removed as they are no longer necessary for visualization, and to avoid soft tissue artifacts associated with these markers.
- The TOE marker is moved from the tip of the big toe to the caput of the 2<sup>nd</sup> metatarsal bone, and is now called MT2.
- Several marker names are changed. STRN marker is now called JN (jugular notch), FLTHI/FRTHI changed to LLTHI/RLTHI, and LATI/RATI are now called LLSHA/RLSHA.
- The placement of the thigh and shank markers has changed.

# 2. Marker set

The HBM uses a marker set containing 46 markers (Figure 1, Table 1) to create a skeleton model and to solve skeleton motion. Each marker is assigned to a certain body segment and has its own weighting for the appropriate segment.

The bold markers in Table 1 and green markers in Figure 1 are anatomical markers needed to define the joint centers and segments of the model during initialization. These markers need to be placed accurately in order to get reliable results. The other markers are technical markers providing redundancy and robustness for the model. Therefore, placement of these markers is less critical. They are also used for the functional calibration of the knee and hip.

Note that the medial markers on the knee and ankle (LMEK, LMM, RMEK, and RMM) can be removed after model initialization since these are only used during initialization to determine joint centers and segment reference frames. This feature was added because these markers often tend to detach during gait.



Figure 1. Front, side, and rear view of the marker set used in the Human Body Model. Green markers are anatomical markers used to define the skeleton during initialization.

\*These markers are optional. If used, they may be removed after model initialization.

Table 1	. Marker placement	of the marker s	etup used in t	he Human	Body	Model.	Bold markers	are anatomic	al markers	used to
define th	ne skeleton during ini	itialization.								

No.	Marker	Position	Placement remarks
1	LHEAD	Left head	Just above the ear, in the middle
2	RHEAD	Right head	Just above the ear, in the middle
3	THEAD	Top head	On top of the head, in line with LHEAD and RHEAD
4	FHEAD	Forehead	On forehead, a bit left from the center
5	C7	C7	On the 7th cervical vertebra
6	T10	T10	On the 10 <sup>th</sup> thoracic vertebra
7	XIPH	Xiphoid process	Xiphoid process of the sternum
8	JN	Jugular notch	On the jugular notch of the sternum
9	LSHO	Left shoulder	On top of the acromion
10	LDELT	Left deltoid muscle	Apex of deltoid muscle
11	LLEE	Left lateral elbow	Lateral epicondyle of the elbow
12	LMEE	Left medial elbow	Medial epicondyle of the elbow
13	LMW	Left medial wrist	On styloid process radius, thumb side
14	LLW	Left lateral wrist	On styloid process ulna, pinky side
15	LFRM	Left forearm	On 1/2 on the line between the LLEE and LMW
16	LFIN	Left fingers	Center of the hand, caput metacarpal 3
17	RSHO	Right shoulder	On top of the acromion
18	RDELT	Right deltoid muscle	Apex of deltoid muscle
19	RLEE	Right lateral elbow	Lateral epicondyle of the elbow
20	RMEE	Right medial elbow	Medial epicondyle of the elbow
21	RMW	Right medial wrist	On styloid process radius, thumb side
22	RLW	Right lateral wrist	On styloid process ulna, pinky side
23	RFRM	Right forearm	On 1/2 on the line between the RLEE and RMW
24	RFIN	Right fingers	Center of the hand, caput metacarpal 3
25	LASIS	Pelvic bone left front	Left anterior superior iliac spine
26	RASIS	Pelvic bone right front	Right anterior superior iliac spine
27	LPSIS	Pelvic bone left back	Right posterior superior iliac spine
28	RPSIS	Pelvic bone right back	Right posterior superior iliac spine
29	LLTHI	Left thigh, lateral	1/2 on the line between the left greater trochanter and LLEK
30	LLEK	Left lateral epicondyle of the knee	On the lateral side of the joint axis

31	LMEK*	Left medial epicondyle of the knee	On the medial side of the joint axis. Check by holding both points and bending the knee; markers should not/hardly move.
32	LLSHA	Left shank, lateral	1/2 on the line between LLEK and LLM
33	LLM	Left lateral malleolus of the ankle	The center of the left lateral malleolus
34	LMM*	Left medial malleolus of the ankle	Most pronounced part of the left medial malleolus
35	LHEE	Left heel	Center of the heel at the same height as LMT2
36	LMT2	Left 2 <sup>nd</sup> meta tarsal	Caput of the 2 <sup>nd</sup> meta tarsal bone, on joint line midfoot/toes
37	LMT5	Left 5 <sup>th</sup> meta tarsal	Caput of the 5 <sup>th</sup> meta tarsal bone, on joint line midfoot/toes
38	RLTHI	Right thigh, lateral	1/2 on the line between the right greater trochanter and LLEK
39	RLEK	Right lateral epicondyle of the knee	On the lateral side of the joint axis
40	RMEK*	Right medial epicondyle of the knee	On the medial side of the joint axis. Check by holding both points and bending the knee; markers should not/hardly move.
41	RLSHA	Right shank, lateral	1/2 on the line between RLEK and RLM
42	RLM	Right lateral malleolus of the ankle	The center of the right lateral malleolus
43	RMM*	Right medial malleolus of the ankle	Most pronounced part of the right medial malleolus
44	RHEE	Right heel	Center of the heel at the same height as RMT2
45	RMT2	Right 2 <sup>nd</sup> meta tarsal	Caput of the 2 <sup>nd</sup> meta tarsal bone, on joint line midfoot/toes
46	RMT5	Right 5 <sup>th</sup> meta tarsal	Caput of the 5 <sup>th</sup> meta tarsal bone, on joint line midfoot/toes

\*These markers are optional. If used, they may be removed after model initialization.

# **3. Model Initialization**

Static initialization of the model is done by recording an initialization pose. Optionally, functional hip and knee joint calibrations can be performed. The functional calibrations have to be performed before the static calibration, to be incorporated in the model. When the static calibration is done prior to the functional calibration, the functional calibration will remain unused until a new static calibration is performed.

For most patients, static model calibration is preferred as functional joint calibration requires the subject to perform complex calibration motions with extensive ranges of motion in both the hip as well as the knee. Recent research also suggests that locating the hip joint center using the Harrington equations generally works as well as, or better than, functional calibration (Peters et al. 2012; Sangeux et al. 2011; Sangeux et al. 2014).

### 3.1 Static Initialization

The static calibration can be done with or without the use of medial knee and ankle markers. In earlier versions of HBM, these medial markers were not included in the marker set. Using the medial markers makes the initialization less pose dependent, which will especially be helpful with subjects who are not able to assume the initialization pose. The calibration without medial markers is still available.

During initialization the position of joint centers, bone lengths, and joint axes are estimated based on:

- Marker coordinates during initialization pose
- Marker diameter [m]
- Knee width [m] (when no medial markers are used)
- Ankle width [m] (when no medial markers are used)

To estimate mass properties of the body segments, the following additional information is needed:

- Subject weight [kg]
- Subject gender

To perform the static initialization, the subject is placed in an initialization pose. The exact execution of the pose is essential when no medial markers are used, since the calibration will be pose dependent in that case. However, even when medial markers are used try to meet the following guidelines as well as possible:

- The subject should stand upright, looking forward, arms about 45 degrees abducted. The direction the subject is facing is not important, since the software automatically compensates for this direction.
- Feet should be pointing forward, approximately at hip width. This can be confirmed by doing knee bends in which the distance between the knees should remain constant.
- Arms and legs must be straight (neutral flexion-extension angle), with palms of the hand facing downwards.

# 3.2 Functional hip joint calibration

A functional hip joint calibration can be performed to determine the joint center of the hip. Subjects should start by standing upright, thereafter; the subject has to perform a star arc movement, which was found to be the movement which leads to the most accurate results according to Camomilla et al. (2006). The star arc movement described in Camomilla et al. (2006) is slightly adapted since excessive hip extension causes significant skin movement artifacts. The adapted star arc consists of five different movements as described below (Figure 2):

- 1. Hip flexion, then back to neutral.
- 2. Combination of hip flexion and abduction, then back to neutral.
- 3. Hip abduction, then back to neutral.
- 4. Combination of hip extension and abduction, then back to neutral.
- 5. A full circumduction movement is made with the hip.



Figure 2. Transverse view of the five movements of the star arc for the calibration of the right hip.

To create as little as possible soft tissue movement in the thigh, subjects should be asked to avoid internal and external rotation of the hip and to minimize frontal rotation of the pelvis (Leardini et al. 1999). Please note that the star motion has to be performed for each leg individually. To use the functional hip calibration, HBM requires a minimal range of motion of 60 degrees of flexion/extension and 30 degrees of abduction (Kainz et al. 2015).

# 3.3 Functional knee joint calibration

Similar to the functional hip joint calibration, subjects should start by standing upright. Subjects should flex and extend the knee about five times through a range of approximately 0 to 90° of flexion. This calibration also needs to be done for each leg individually.

# **4. Skeleton Model**

The skeleton model is designed for real-time biomechanical analysis of the human body, and involves all kinematic degrees of freedom (DOF) which are controlled by muscles. The trunk is modeled as two segments which are coupled to give three degrees of freedom. Figure 3 shows the 18-segment skeleton model, which has a total of 46 DOF.



**Figure 3.** Hierarchy of the skeleton model: The pelvis is the root segment, which has six degrees of freedom (DOF) relative to the world. Numbers besides the segments represent the DOF added by that segment. The two DOFs of ankle and subtalar joint are combined in this diagram. The total number of DOF of the skeleton model is 46.

HBM generates the following list of body segment names:

- Pelvis
- Abdomen
- Thorax
- Head
- RUpperArm
- LUpperArm
- RForeArm
- LForeArm
- RHand
- LHand
- RFemur
- LFemur
- RShank
- LShank
- RFoot
- LFoot
- RToe
- LToe

For each segment a reference frame is needed to define the equations of motion (Figure 4). These segment reference frames are defined only once during model initialization. Thereafter, the segments' marker coordinates and joint centers are expressed as constants relative to these reference frames. During motion, the markers and joints define skeleton motion via the inverse kinematics as described in Section 5.1.

As a general principle, the origin of each segment is placed in the proximal joint (i.e. the connection onto the parent bone), except for pelvis, which is the root of the hierarchy. As a general rule, the segment Z-axis is defined to go through its distal joint (when available). This is also consistent with de Leva (1996), so that the local X- and Y-coordinates of the center of mass, for all segments, are zero. The segment Z-axis will generally point up when standing upright. This means the centers of mass in the arm and leg segments have negative Z-coordinates. The advantage of defining the Z-axis this way is that the model stands perfectly straight when all rotations are zero (except in the ankles). Rotations are then easier to interpret.

Joint axes are defined so that kinematic data are compatible with clinical definitions. These are based on the ISB standards (Wu et al. 1995, 2002, 2005), unless when these are not practical for clinical use.

Joint axes are also needed to constrain the motion of the model, so that the model represents muscle function, and not the small motions (e.g. knee abduction and rotation, joint translations) that are not controlled by muscles.

The remainder of this section describes the definitions of the segments and how these are constructed during the model initialization. As the origin of each segment is placed in the proximal joint, the segments are described bottom up starting with most distal joint (the foot) working back up towards the parent segment and end with the trunk. For each segment the construction of the proximal joint center is described first, as this will be the origin for the segment reference frame (which is described second). Finally the joint axes and joint angles are described.

#### 4.1 Foot

#### Joint centers

#### Ankle joint

The ankle joint center is assumed to be the midpoint between the lateral and medial malleolus. If both lateral and medial ankle markers are available, the ankle joint center is defined as midpoint between these two markers. When no medial malleolus marker is used, the ankle joint center will be defined as 'half of ankle width + marker radius' medial to the lateral marker. Medial direction in this case is a horizontal projection of the vector from RASIS to LASIS.

#### Subtalar joint

According to van den Bogert et al. (1994) the subtalar joint center is defined 12mm below the ankle joint center. In HBM, this is implemented as a displacement along the X-axis of the foot. This proposed 12mm was scaled by tibia length as follows:

Tibia length / 0.375 \* 12

in which tibia length is the distance between lateral knee and ankle markers.

#### Reference frame

The origin of the foot is located in the subtalar joint center. The Z-axis is parallel to the vector from MT2 to HEE markers (which should be horizontally when the foot is flat on the ground) and points posteriorly. In this way HBM will report a 90° flexion angle when standing in neutral pose. The X-axis is based on the Z-axis and a temporal Y-axis, for which two possibilities exist, depending on the presence of the medial ankle marker. When a medial marker is present, a temporal Y-axis between the lateral and medial malleolus pointing to the left is defined. In case the medial marker is not present, the temporal Y-axis is parallel to the line between the two ASIS markers and pointing to the left. The X-axis is the cross product of the temporal Y-axis and the Z-axis, and will point dorsally. The Y-axis is the cross product of the Z- and X-axis.

#### Joint axes and joint angles (degrees of freedom)

The ankle is modeled as two hinges, based on Isman's normative data (Isman & Inman 1969; van den Bogert et al. 1994). Using three hinges would lead to overestimation of muscle forces as in Burdett (1982), a problem nicely described by Glitsch & Baumann (1997). Between the two joint axes a distance of 12 mm is assumed according to van den Bogert et al. (1994) which is scaled in HBM by tibia length as mentioned above. A talus segment is not explicitly defined, since its mass can be ignored and only has a kinematic role. The ankle thus has two degrees of freedom, which are plantar flexion (rotation about the Y-axis of the shank reference frame; plantar flexion is positive) and pronation/supination (rotation about the pronation/supination axis; pronation is positive). The pronation/supination axis is not aligned with the foot coordinate axes, but is defined in the foot reference frame using the average subtalar joint (STJ) in Isman & Inman (1969) and points forward. According to Isman and Inman, the STJ is inclined 42 degrees from the horizontal plane, and deviates 23 degrees medially from the sagittal plane. Therefore, our STJ axis is for the right foot:

 $STJ = \begin{bmatrix} \cos(42^\circ)\cos(23^\circ)\\ \cos(42^\circ)\sin(23^\circ)\\ \sin(42^\circ) \end{bmatrix}$ 

### 4.2 Shank

#### Knee joint center

Three different methods can be used to determine the knee joint center. Two different methods for static initialization are available, and one method is available for functional knee calibration. The knee joint center is assumed to be the midpoint between the lateral and medial epicondyle. If both lateral and medial knee markers are available during static initialization, the knee joint center is defined as midpoint between these two markers. When no medial knee marker is used, the knee joint center will be defined as 'half of knee width + marker radius' medial to the lateral marker. Medial direction in this case is a horizontal projection of the vector from RASIS to LASIS.

In case of functional knee calibration, knee axes are estimated using the axis of rotation estimation method by Gamage & Lasenby (2002), as was recommended by van Campen et al. (2011) and MacWilliams (2008). This method assumes that the markers on the shank (LM, MM, and LSHA) rotate about a fixed axis of rotation relatively to the thigh. A least squares cost function is used to find the best fitting axis. The knee joint center is defined as the projection of the midpoint between the medial and lateral epicondyle onto this axis.

#### Reference frame

The origin of the shank is located in the knee joint center. The negative Z-axis points towards the ankle joint center. A temporal Y-axis is constructed along the ankle axis and points to the left (see section 4.1). The X-axis is the cross product of the Z-axis and the temporal Y-axis. The Y-axis is the cross product of the Z- and X-axis to ensure orthonormality.

#### Joint axes and joint angles (degrees of freedom)

The knee is modeled as one hinge, since Glitsch & Baumann (1997) have shown that this is best for the analysis of muscle function and estimation of muscle forces. Also, the abduction/adduction range of motion is very small. As to internal/external rotation, the knee does have a 45 degrees range of motion when flexed 90 degrees. During gait however, the knee is extended so there will be little internal/external rotation. Therefore, modeling these movements would most likely reflect inherent crosstalk errors in the 3D kinematic calculations, rather than a true anatomical movement (Ramakrishnan & Kadaba 1991). Thus, the knee has one degree of freedom, which is flexion/extension (rotation around the Y-axis; flexion is positive). Ab/adduction and internal/external rotation angles are constant, set during initialization.

### 4.3 Thigh

#### Hip joint center

A predictive method has to be used to determine the hip joint center (HJC) in case of the static model initialization, while a functional approach is used in case of functional hip calibration. Several studies comparing different methods of HJC estimation (Assi et al. 2016; Kainz et al. 2016; Peters et al. 2012; Sangeux et al. 2011; Sangeux et al. 2014) showed that the method of Harrington et al. (2007) is the most accurate predictive method.

The most accurate functional approach was found to be the geometric sphere fit method by Gamage and Lasenby (2002) (Kainz et al. 2015; MacWilliams 2008; Sangeux et al. Baker 2011; Sangeux et al. 2014). Hence, these two methods are implemented in the HBM.

#### Harrington equations

The Harrington equations (Harrington et al. 2007) are linear regression equations to predict the location of the HJC based on pelvic width and pelvic depth. Pelvic width is defined as the distance between the two ASIS markers, while pelvic depth is defined as the distance between the midpoints of the line segments connecting the two ASIS and the two PSIS.

#### Geometric sphere fit

The "bias compensated least squares method" by Halvorsen (2003), based on the geometric sphere fit method by Gamage and Lasenby (2002) is used to estimate the HJC. This method assumes that each marker on the thigh (LTHI, LEK, and MEK) is moving along a trajectory

on the surface of a sphere with the center at the HJC. The location of the HJC is estimated based on these markers during an iterative algorithm, in which a correction for the bias due to measurement noise is performed every iteration until convergence is reached.

#### Reference frame

The origin of the thigh is located at the hip joint center. The negative Z-axis points towards the knee joint center. A temporal Y-axis is constructed along the knee axis and points to the left. When only static model initialization is used, this is a vector through the lateral epicondyle and the knee joint center. Note that when medial markers are used to determine the knee joint center, a misplacement of these markers will result in a rotated thigh reference frame. This in turn will result in an offset in the internal or external hip rotation. In case of the functional knee calibration, the temporal Y-axis is along the functional axis of rotation. The X-axis is the cross product of the Z-axis and the temporal Y-axis. The Y-axis is the cross product of the Z-axis.

#### Joint axes and joint angles (degrees of freedom)

The hip has three degrees of freedom, which are rotations around the Y-axis (hip flexion; flexion is positive), X-axis (hip ab/adduction; adduction is positive), and Z-axis (hip rotation; internal rotation is positive).

### 4.4 Pelvis

#### Reference frame

The origin of the pelvis is defined as the midpoint between the two ASIS markers. The Y-axis is defined as the vector from RASIS to LASIS. The Z-axis is the cross product of the Y-axis and a temporal X-axis, which is a vector from the midpoint between the two PSIS markers to the midpoint between the two ASIS markers. Subsequently, the X-axis is the cross product of Y and Z.

#### Joint axes and joint angles (degrees of freedom)

The pelvis has six degrees of freedom relative to the ground, which are implemented as three global translations (X, Y, and Z) of the pelvis origin, and rotations about the Y-axis (pelvic tilt; forward tilt is positive), X-axis (pelvic obliquity; Left drop/right lift is positive), and Z-axis (pelvic rotation; left twist is positive).

### 4.5 Trunk

The trunk is modeled as two rigid segments for which statistical models were used that predict mass properties (de Leva 1996). These segments are coupled so that there are only three degrees of freedom. This allows the trunk to flex, bend, and twist realistically without having to solve extra degrees of freedom which would be noisy and sensitive to marker wobble due to soft tissue artifacts.

#### Joint centers

#### S1/L5 joint

The joint center of the S1/L5 joint (joint between pelvis and trunk) is defined based on the data from Reynolds et al. (1982) and as described by the algorithm below. The algorithm calculates the joint center based on pelvic width and pelvic depth, which are calculated from

the pelvic markers. Due to the anatomical differences between the male and female pelvis, the algorithm provides different calculations according to gender. Note that the algorithm below is expressed in a reference frame in which X is anterior, Y is to the left, and Z is up are assumed.

 $Y_{S1L5} = 0$ 

For male subjects:  $X_{S1L5} = X_{midASIS} - 0.498888 * pelvic_depth$  $Z_{S1L5} = Z_{midASIS} + 0.111790 * pelvic_width$ 

For female subjects:

 $X_{S1L5} = X_{midASIS} - 0.543004 * pelvic_depth$  $Z_{S1L5} = Z_{midASIS} + 0.102756 * pelvic_width$ 

#### Superior trunk joint

The joint center of the proximal trunk joint (joint between abdomen and thorax segments) is located at the T10-T11 joint. The location of the T10-T11 joint is defined at 26% along the vector from T10 to XIPH as derived from an OpenSim model of the full thoracolumbar spine and ribcage (Bruno et al. 2015).

#### Segment reference frames

#### Abdomen

The origin of the abdomen is located in the S1/L5 joint center. The Z-axis points to the superior trunk joint. The X-axis is the cross product of the Z-axis and the pelvic Y-axis. The Y-axis is the cross product of the Z- axis and X-axis.

#### Thorax

The origin of the thorax is located in the superior trunk joint center. The Z-axis is a vector connecting the midpoint between XIPH and T10 and the midpoint between JN and C7. The Y-axis is a vector perpendicular to the plane formed by JN, C7, and the midpoint between XIPH and T10, pointing to the left. The X-axis is the cross product of the Y and Z-axis, pointing anteriorly.

#### Joint axes and joint angles (degrees of freedom)

The trunk has three degrees of freedom, which are rotations about the Y-axis (trunk tilt; forward lean is positive), X-axis (trunk lateroflexion; right lean is positive), and Z-axis (trunk rotation; left twist is positive).

### 4.6 Upper arm

The upper arms are attached to upper trunk with six DOFs: 3 translations and 3 rotations. This allows all possible shoulder motions.

#### Shoulder joint center

The shoulder joint center is defined 35 mm below the SHO marker (de Leva 1996).

#### Segment reference frame

The origin of the upper arm is located at the shoulder joint center. The negative Z-axis points towards the elbow joint center. The X-axis points anterior and is the cross-product of the Z-axis and the mediolateral vector which is a horizontal projection of the vector from RASIS to LASIS. The Y-axis is the cross product of the Z-axis and X-axis.

#### Joint axes and joint angles (degrees of freedom)

Helical angles are used (Woltring 1994) to parameterize shoulder rotation. The helical axis is expressed in the Thorax reference frame, such that the components can be interpreted as flexion, abduction, and internal rotation.

### 4.7 Forearm

#### Elbow joint center

The elbow joint center is the midpoint between the LEE and MEE markers.

#### Segment reference frame

The origin of the forearm is located in the elbow joint center. The negative Z points towards the wrist joint center. The X-axis points anterior and is the cross-product of the Z-axis and the mediolateral vector which is a horizontal projection of the vector from RASIS to LASIS. The Y-axis is the cross product of the Z-axis and X-axis.

#### Joint axes and joint angles (degrees of freedom)

The forearm has two degrees of freedom, which are rotation around the Y-axis (elbow flexion/extension; flexion is positive), and rotation around the Z-axis (pronation/supination; pronation is positive). The rotation around the X-axis is set to a constant angle, determined during the initialization pose.

### 4.8 Hand

#### Wrist joint center

The wrist joint center is the midpoint between the MW and LW markers.

#### Segment reference frame

The origin of the hand is located in the wrist joint center. All axes are aligned with the axes of the forearm (hence it is important that subjects have neutral wrist angles during the initialization pose).

#### Joint axes and joint angles (degrees of freedom)

The wrist has two degrees of freedom, which are rotations around the X-axis (flexion/extension; flexion is positive), and rotations around the Y-axis (ab-/adduction; abduction is positive). The rotation around the Z-axis is set to a constant angle, determined during the initialization pose.

#### 4.9 Head

#### Neck joint center

The neck is modeled as a single spherical joint. According to de Leva (1996), the neck rotation center is at the spine at the level of the chin. This is defined to be on the trunk

midline (line from S1/L5 to mid-shoulder point during initialization pose), 2 cm above the level of C7.

#### Segment reference frame

The origin of the head segment is located in the neck joint. The Z-axis points from neck joint to THEAD. The X-axis is the cross-product of the Z-axis and the vector from RHEAD to LHEAD, pointing anterior. The Y-axis is the cross product of the Z-axis and X-axis.

#### Joint axes and joint angles (degrees of freedom)

As the head is attached to the upper trunk via a single spherical joint, there are three degrees of freedom, which are rotations around the Y-axis (head flexion/extension; flexion is positive), the X-axis (head bend; right bend is positive), and the Z-axis (head twist; left twist is positive).



**Figure 4**. Front view of segment reference frames used in the low er limb HBM. X-, Y-, and Z-axes are indicated by red, green, and blue arrows, respectively. Segment origins generally are located at the proximal joint center, and negative Z-axes go through the distal joint center when available (except for the pelvis). The Z-axes of the feet point posteriorly.

# 4.10 Mass properties

During subject initialization, mass properties of each body segment are estimated based on segment lengths (distance between joint centers), gender, and total body mass. Segment mass, location of the center of mass, and the inertia tensor of each segment are estimated using parameters from Table 4 from de Leva (1996) which provides the following information:

- Segment mass as a percentage of total body mass: mperc
- Segment center of mass location as a percentage of segment length: cmperc
- Radii of gyration for the sagittal, frontal and transversal plane, expressed as a percentage of segment length: rsag, rfro, rtra.

Segment mass ( $m_{segment}$ ) is calculated from *mperc* and the total body mass ( $m_{total}$ ):

$$m_{segment} = \frac{mperc}{100} * m_{total} \tag{1}$$

The center of mass of a given segment ( $\vec{r}_{CM}$ ) is expressed in the segment's reference frame and is located on the longitudinal axis:

$$\vec{r}_{CM} = \frac{cmperc}{100} \begin{bmatrix} 0\\0\\1 \end{bmatrix}$$
(2)

Inertia tensors for each segment are also expressed in the segment's reference frame:

$$\mathbf{I} = m_{segment} \left(\frac{L_{segment}}{100}\right)^2 \begin{bmatrix} rsag^2 & 0 & 0\\ 0 & rfro^2 & 0\\ 0 & 0 & rtra^2 \end{bmatrix}$$
(3)

In which  $L_{segment}$  is the length of the segment.

The total body center of mass is calculated by taking the weighted average of the segment centers of mass.

# 5. Biomechanical Analysis

Biomechanical analysis in HBM is done in five steps. First, inverse kinematics is used to describe skeletal motion. Second, the data is low pass filtered which is needed to calculate the first and second derivative (velocity and acceleration) without too much noise. Third, an inverse dynamics analysis is performed to calculate the generalized forces (forces and moments actuating the degrees of freedom). In the two final steps muscles moment arms and muscle forces are estimated.

# 5.1 Kinematics

#### Kinematic degrees of freedom

Based on the segment description in section 4, there are 46 kinematic degrees of freedom, and they have been given the following names. Each degree of freedom has a kinematic variable associated with it. These are also known as "generalized coordinates".

- PelvisX
- PelvisY
- PelvisZ
- PelvisYaw
- PelvisForwardPitch
- PelvisRightRoll
- TrunkFlexion
- TrunkRightBend
- TrunkLeftTwist
- HeadFlexion
- HeadRightBend
- HeadLeftTwist
- RShoulderUp
- RShoulderForward
- RShoulderInward
- RShoulderFlexion
- RShoulderAbduction
- RSchoulderInternalRotation
- RElbowFlexion
- RForeArmPronation
- RWristFlexion
- RHandAbduction
- LShoulderUp
- LShoulderForward
- LShoulderInward
- LShoulderFlexion
- LShoulderAbduction
- LSchoulderInternalRotation
- LElbowFlexion
- LForeArmPronation
- LWristFlexion

- LHandAbduction
- RHipFlexion
- RHipAbduction
- RHipInternalRotation
- RkneeFlexion
- RAnklePlantarFlexion
- RFootPronation
- RToeFlexion
- LHipFlexion
- LHipAbduction
- LHipInternalRotation
- LKneeFlexion
- LAnklePlantarFlexion
- LFootPronation
- LToeFlexion

#### Inverse kinematics

In contrast to conventional models that calculate each segment independently using at least three markers per segment, the inverse kinematics in HBM are calculated all at once. During static calibration HBM determines the segment reference frames based on the marker positions. For each real-time frame these segments are fitted onto the marker data by minimizing the error between the marker data and the segment orientations. Because all available markers are used in this optimization, fewer markers are required per segment than in the conventional models. Technically HBM would only require the anatomical markers (bold in Table 1) to solve kinematics. However, additional technical markers are added to HBM (Table 1) to provide redundancy and robustness for the model in case of marker drop outs.

The inverse kinematics is based on van den Bogert & Su (2008). The skeleton model is defined with 46 DOF, represented by the generalized coordinates  $q = [q_1 \dots q_{21}]^T$ , in which for example  $q_1$  is PelvisX,  $q_2$  is PelvisY, etcetera (see above). Since all segment reference frames are known from the marker data, the position vector  $r = [x, y, z]^T$  and orientation matrix R of each segment expressed in the global reference frame can be computed as a function of q. Furthermore, the position of each marker in the segment reference frame (p) is known. Therefore, the coordinates of each marker in the global reference frame can be expressed as a function of q, by adding  $R(q) \cdot p$  (i.e. the position vector of the segment reference frame, rotated to the global reference frame) to the position vector of the segment origin in the global reference frame (r(q)). Thus, the position of a certain marker i in the global reference frame is

$$\boldsymbol{r}_i = \boldsymbol{r}(\boldsymbol{q}) + \boldsymbol{R}(\boldsymbol{q}) \cdot \boldsymbol{p}_i \equiv \boldsymbol{f}_i(\boldsymbol{q})$$

The optimal estimate for the skeleton pose q can then be obtained by minimizing the squared difference between the measured coordinates of the markers in the global reference frame and their position expressed as a function of q. If M markers are placed, the optimization is

(5)

$$F(q) = \sum_{i=1}^{M} ||r_i - f_i(q)||^2$$

Note that in three dimensions, the right hand side is a sum of 3M squares, since the squares of x, y, and z distances are added. This optimization method is known as global optimization (Lu & O'Connor 1999), in which global refers to the fact that the entire skeleton is modeled at once, instead of modeling each segment individually. This makes the model less sensitive to marker drop-outs and skin artifacts. In HBM, equation 6 is minimized using the Levenberg-Marquardt algorithm, adapted from Numerical Recipes (Press et al. 1992). In this way, the generalized coordinates (q) for each frame are calculated within 1ms of computation time.

#### Filtering and differentiation

The calculation of joint moments and muscle forces depends on the acceleration and velocity of the skeleton, which are the first and second derivative of skeleton movement (q). To prevent these derivatives from being too noisy, q has to be smoothed using a filter.

The HBM software has a built-in real-time 2<sup>nd</sup> order low pass Butterworth filter. Higher order filters may reject noise better, but will also increase the time delay. Therefore, the used filter is considered to be a good compromise to be used in HBM. The state variable technique is used instead of the more common recursive digital filter, which allows processing data with varying sample rates (which occurs if the motion capture system drops a frame). Furthermore, this technique automatically generates first and second derivatives.

The cutoff frequency of the filter can be adjusted by the user to a maximum of 20 Hz. Higher frequencies are not allowed because these are unnecessary for human movement and would increase computation time. The default cutoff frequency is set to 6Hz, since this was found to be the highest frequency in kinematics related to gait (Winter et al. 1974). To prevent artifacts in joint movements, force plate data are processed with the same low pass filter as the kinematics (van den Bogert & De Koning 1996; Bisseling & Hof 2006).

# 5.2 Kinetics

#### **Generalized forces**

Each DOF is actuated with a force (for translational DOFs) or moment (for rotational DOFs). These forces and moments are also known as "generalized forces". The signs of these are defined such that a positive force or moment would generate a movement in which the corresponding generalized coordinate is increasing. These (internal) moments and forces are solved using inverse dynamics. Furthermore, mechanical work can be computed as the product of the amount of change in the generalized coordinate and the amount of generalized force. The powers are presented per joint axis as most of the literature that reports on joint power presents a 2D sagittal plane analysis. When comparing HBM results with those results, only the flexion-extension power should be used. If preferred, the individual powers per joint can easily be summed to calculate the total joint power since they are scalars.

There is one exception to the correspondence between generalized coordinates and generalized forces: pelvis moments have been defined as Cartesian XYZ components in the world reference frame, rather than as moments on the yaw, pitch, and roll axes. Thus, the first six generalized forces are residual loads exerted by the outside world on the pelvis.

When all external forces are measured and accounted for in the inverse dynamics, these loads should be zero.

#### Inverse dynamics

The generalized forces are calculated in an inverse dynamic analysis, which has the low pass filtered kinematics and the ground reaction forces as input. Like the inverse kinematic solution does for the generalized coordinates, the inverse dynamic analysis calculates all generalized forces ( $\tau$ ) at once using the following equation from van den Bogert et al. (2013):

$$\tau = M(q)\ddot{q} + c(q,\dot{q}) + B(q)\tau_{ext}$$
(7)

In this equation *M* is a square matrix containing mass properties of the segments, *c* are terms related to Coriolis and centrifugal effects and gravity, and  $B(q)\tau_{ext}$  are the measured external forces (force plate data).

It is assumed that full ground reaction force data is available. When two force plates are used and each plate registers 3D forces and 3D moments,  $\tau_{ext}$  contains 12 variables. Furthermore it is assumed that all DOFs of the model are actuated, which implies that  $\tau$  contains one variable for each DOF of the model. Thus, the solution also includes 3D force and moment acting on the root segment (pelvis). These values will be non-zero, even though it is known these values are exactly zero. Allowing this error has the advantage that there is an exact solution for  $\tau$ . Also, joint moments are only influenced by inertial effects distal to the joint.

# 5.3 Muscle properties

HBM includes 43 lower limb muscles (for each limb, Table 2) which are modeled according the Gait2392 model (Delp et al. 2007) which uses joint definitions adopted from Delp et al. (1990). A set of shoulder and arm muscles using the model described by Chadwick et al. (2009) is also included. This model includes 22 muscles for each arm. However, in order to represent the function of large muscles correctly, these are separated into parallel muscle elements. Therefore, 102 muscle elements are present in each arm. The trunk muscles are modeled according to the model of Lambrecht et al. (2009), which adds 10 trunk muscles to the model (Table 4). This model also provided trunk function for six musles that were already in the set of arm and leg muscles (L\_Psoas, R\_Psoas, L\_LatissimusDorsi5, R\_LatissimusDorsi6, R\_LatissimusDorsi6).

For each muscle maximal isometric force ( $F_{max}$ ), and polynomial equations for muscle length as a function of joint angles are available. HBM is able to estimate muscle force (F) and activation level ( $F/F_{max}$ ) using these parameters and skeletal pose.

Lower limb muscles in HBM	
Gluteus Medius 1	Psoas
Gluteus Medius 2	Quadratis Femoris
Gluteus Medius 3	Gemelli
Gluteus Minimus 1	Piriformis
Gluteus Minimus 2	Rectus Femoris

 Table 2. Low er limb muscles included in the HBM.

Gluteus Minimus 3	Biceps Femoris SH
Semimembranosus	Vastus Medialis
Semitendinosus	Vastus Intermedius
Biceps Femoris LH	Vastus Lateralis
Sartorius	Medial Gastrocnemius
Adductor Longus	Lateral Gastrocnemius
Adductor Brevis	Soleus
Adductor Magnus 1	Tibialis Posterior
Adductor Magnus 2	Flexor Digitorum Longus
Adductor Magnus 3	Flexor Hallicus Longus
Tensor Fascia Lata	Tibialis Anterior
Pectineus	Peroneus Brevis
Gracilis	Peroneus Longus
Gluteus Maximus 1	Peroneus Tertius
Gluteus Maximus 2	Extensor Digitorum Longus
Gluteus Maximus 3	Extensor Hallicus Longus
lliacus	

#### Table 3. Upper limb muscles included in the HBM

Upper limb muscles in HBM	
DeltoidScapular1	TricepsLH3
DeltoidScapular2	TricepsLH4
DeltoidScapular3	LatissimusDorsi1
DeltoidScapular4	LatissimusDorsi2
DeltoidScapular5	LatissimusDorsi3
DeltoidScapular6	LatissimusDorsi4
DeltoidScapular7	LatissimusDorsi5
DeltoidScapular8	LatissimusDorsi6
DeltoidScapular9	PectoralisMajorTH1
DeltoidScapular10	PectoralisMajorTH2
DeltoidScapular11	PectoralisMajorTH3
DeltoidClavicular1	PectoralisMajorTH4
DeltoidClavicular2	PectoralisMajorTH5
DeltoidClavicular3	PectoralisMajorTH6

DeltoidClavicular4	PectoralisMajorCH1
CoracoBrachialis1	PectoralisMajorCH2
CoracoBrachialis2	TricepsMedH1
CoracoBrachialis3	TricepsMedH2
Infraspinatus1	TricepsMedH3
Infraspinatus2	TricepsMedH4
Infraspinatus3	TricepsMedH5
Infraspinatus4	Brachialis1
Infraspinatus5	Brachialis2
Infraspinatus6	Brachialis3
TeresMinor1	Brachialis4
TeresMinor2	Brachialis5
TeresMinor3	Brachialis6
TeresMajor1	Brachialis7
TeresMajor2	Brachioradialis1
TeresMajor3	Brachioradialis2
TeresMajor4	Brachioradialis3
Supraspinatus1	PronatorTeres1
Supraspinatus2	PronatorTeres2
Supraspinatus3	Supinator1
Supraspinatus4	Supinator2
Subscapularis1	Supinator3
Subscapularis2	Supinator4
Subscapularis3	Supinator5
Subscapularis4	PronatorQuadratus1
Subscapularis5	PronatorQuadratus2
Subscapularis6	PronatorQuadratus3
Subscapularis7	TricepsLatH1
Subscapularis8	TricepsLatH2
Subscapularis9	TricepsLatH3
Subscapularis10	TricepsLatH4
Subscapularis11	TricepsLatH5
BicepsBrachiiLH	Anconeus1
BicepsBrachiiSH1	Anconeus2

BicepsBrachiiSH2	Anconeus3
TricepsLH1	Anconeus4
TricepsLH2	Anconeus5

Table 4. Trunk muscles in the HBM

Trunk muscles in HBM	
L_ErectorSpinae	R_ObliqueInternal
R_ErectorSpinae	L_QuadratusLumborum
L_ObliqueExternal	R_QuadratusLumborum
R_ObliqueExternal	L_RectusAbdominis
L_ObliqueInternal	R_RectusAbdominis

#### Muscle moment arms

Muscle moment arms were estimated using the method of van den Bogert et al. (2013). In this method the coupling between muscles and skeleton is represented by a polynomial function which describes muscle length as a function of skeleton pose.

$$L(q) = \sum_{i=1}^{N_{terms}} c_i \prod_{j=1}^{N_{DOF}} q_j^{e_{ij}}$$
(8)

In this equation,  $N_{terms}$  is the number of polynomial terms,  $q_1 \dots q_{N_{DOF}}$  are values of the joint angles between origin and insertion of the muscle. The coefficients  $c_i$ , and the exponents  $e_{ij}$  are the model parameters.

The moment arm  $d_k$  can be obtained by partial differentiation with respect to the  $k^{\text{th}}$  joint angle as was described by An et al. (1984).

$$d_k(\boldsymbol{q}) = \frac{\partial L}{\partial q_k} = \sum_{i=1}^{N_{terms}} c_i e_{ik} \prod_{j=1}^{N_{DOF}} q_j^{e_{ij} - \delta_{jk}}$$
(9)

The model was loaded into OpenSim (Delp et al. 2007), in which the skeleton was systematically moved through many combinations of joint angles. For each skeleton pose, moment arms of all muscles and the corresponding joint angles were exported to a database. A stepwise regression was then used to fit the model to these data, in order to obtain values of the model parameters  $c_i$  and  $e_{ij}$ .

#### Muscle force estimation

A matrix D(q) is constructed which contains muscle moment arms of all muscles with respect to all generalized coordinates. Since all moment arms  $(d_k)$  and all joint moments  $(\tau)$  are known, muscle forces (*F*) can be estimated. This is done for all muscles at once using a static optimization which minimizes the squared activation levels (equation 10) (van der Helm 1994), while satisfying the known joint moments  $\tau$ . The optimization is weighted by muscle volume ( $V_i$ ) to make the solutions independent of the level of discretization of the muscular anatomy (van den Bogert et al. 2013; Holmberg and Klarbring 2012). Muscle volumes were assumed to be proportional to the product of maximal force and fiber length. These muscle properties were taken from the original models (Chadwick et al. 2009; Delp et al. 1990; Lambrecht et al. 2009).

$$\boldsymbol{F} = \sum_{i=1}^{n} V_i \left(\frac{F_i}{F_{max}}\right)^2 \tag{10}$$

Subject to linear equality constraints  $D(q)F = \tau$ And bound constraints  $F_i \ge 0$ 

This is a quadratic programming problem, which is solved in HBM in real time using a recurrent neural network as described by Xia & Feng (2005).

Activation levels are guaranteed to be positive, but are not guaranteed to be less than 1. The  $F_{max}$  values used in the optimization are derived from cadaveric data (Delp et al. 1990). These values are meant to be interpreted as relative muscle strengths, so activation levels may be higher than 1 when capturing above average strong subjects.

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